

RESEARCH ARTICLE

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# Automatic design algorithms for securing the ground contact stability of mobile cranes

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## Abstract

**Background:** Mobile cranes overturn due to excessive lifting, heavy wind, or when appropriate ground contact pressure is not secured. Such accidents can be prevented by reviewing the force conveyed from the outrigger to the ground upon lifting, as well as the soil bearing force. The stability review of mobile crane overturn is classified into the following stages: reviewing lifting conditions, mobile crane selection and reviewing ground contact stability. However, a precise review of ground contact stability requires expertise and is extremely time-consuming. Thus, this study develops automatic design algorithms for securing the ground stability of mobile cranes for easy and quick stability reviews.

**Methods:** The stability review method and the algorithm models are created in connection with the proposed conceptual process. The algorithms proposed in this study conduct simulations for all possible candidate cases, save the results in a database, review practical alternatives, and select the solution that minimizes cost. To verify the effectiveness of the automatic design model, a case project was selected and the algorithm was applied assuming several conditions.

**Results:** Developed algorithms can select candidate cranes according to lifting conditions and design plates through simulations easily and quickly, and design components required for ground contact plate design are collected to build the database that allows easier and quicker stability review.

**Conclusion:** The algorithms proposed in this study conduct simulations for all possible candidate cases, save the results in a database, review practical alternatives, and select the solution that minimizes cost. Developed processes are useful for analyzing correlations of mobile crane performance, ground contact and soil bearing force reinforcement designs and so forth, and for systematically selecting optimal mobile cranes.

**Keywords:** Mobile crane; Stability; Lifting plan; Ground contact pressure; Automatic design model

## Background

Many crane accidents occur globally, including the overturn of mobile cranes in Phuket, Thailand and England (The Vertikal Press 2014). As the use of cranes increases in South Korea, the number of overturn accidents is gradually increasing, and accidents related to mobile cranes account for approximately 61.4% of all crane accidents (Kim and Lee 2007). Overturn of mobile cranes occurs due to excessive lifting, heavy wind, or when appropriate ground contact pressure is not secured. Such accidents can be minimized by reviewing the force that is conveyed from the outrigger to the ground upon lifting

and the soil bearing force. The stability review of mobile crane overturn is classified into the following stages: reviewing lifting conditions, mobile crane selection, and reviewing ground contact stability. For safe operation, stage-by-stage reviews are needed.

Stability should be pre-reviewed, and it is reasonable to select mobile cranes among the candidate cranes that have completed reviews in consideration of cost or other factors. However, engineers or technicians do not set lifting plans that suit the construction conditions for stability analyses when implementing construction projects; instead, equipment is operated based on the information provided by an equipment supplier. Operation relying on such limited information and experience is the fundamental cause of crane disasters (Ho, Han and Kim 2007). In

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addition, since such an approach makes precise reviews of mobile cranes and working conditions impossible, it is difficult to select the optimal mobile crane.

There are two factors that prevent engineers or technicians from setting detailed mobile plans. First, it is difficult and extremely time-consuming to consider the ground contact stability applied to mobile cranes. Second, there is not enough of a systematic technique for analyzing a lot of data for stability review of candidates. There have been previous studies that investigated the selection of optimal cranes, taking into account the lifting capacity of mobile cranes and transporting routes (Reddy and Koshy 2002; Al-Hussein et al. 2001; Tantisevi and Burcu 2007). However, those previous studies did not include detailed stability reviews such as the soil bearing force and ground reinforcement. Therefore, this study intends to move beyond the limits of previous studies and develop automatic design algorithms for securing the ground contact stability of mobile cranes. The algorithms proposed in this study focus on the ground stability review process of mobile cranes.

For stability review of cranes, this study limits scope to improve the efficiency of the study and the reliability of its results. Above all, the study subject is limited to the hydraulic crane (or tire crane) that uses an outrigger among mobile cranes. The lifting method can be divided into single lifting and double lifting, and the study is conducted assuming single lifting. In the case of double lifting, more than two working radii and the soil bearing force should be reviewed, and the distance from the crane should be considered. Thus, double lifting has a different method of stability review, and an additional study should be carried out based on this study result. Also, as shown in Figure 1, the study reviews the ground contact stability. The range of reinforcement of soil bearing force occurs when the crane is installed on soil or ground, and this study excludes cases in which it is installed on top of a structure. The reinforcement of structure has a different procedure for reviewing bending, shearing, and sagging compared to that of soil or ground, so it requires a different model. Lastly, the study is

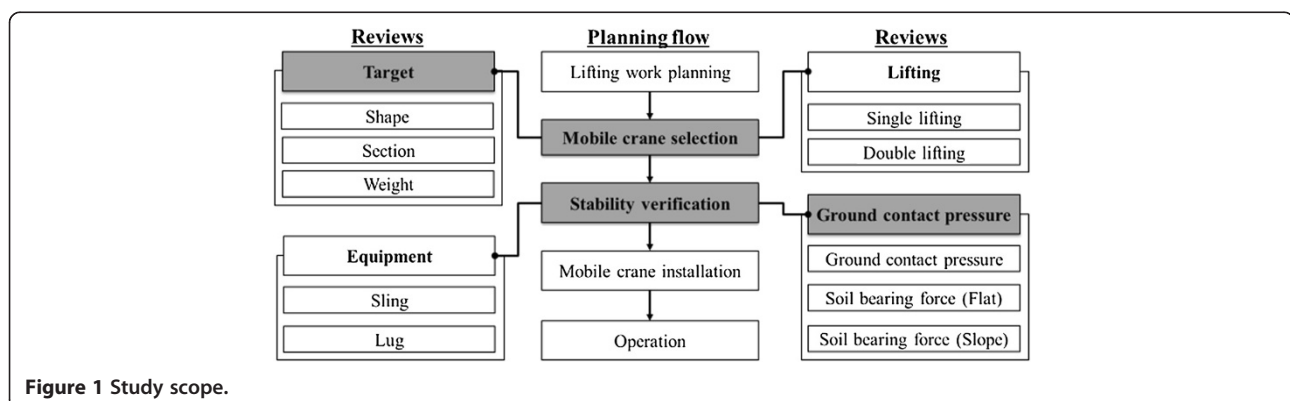
conducted assuming that the boom, sling, and lug meet the lifting requirements, and there is no stability review for each of these materials.

## Methods

To achieve the objective of this study, first, ground contact stability review items are identified and a conceptual process is developed. Second, the conceptual process for reinforcing ground contact pressure and soil bearing force is proposed. Third, a stability review method and algorithm models are created in connection with the proposed conceptual process. Finally, automatic models among the created models are developed, taking into account safety and economic feasibility. The developed processes analyzes correlations among the performance of mobile cranes, ground contact, and soil bearing force reinforcement and so on in order to assist the systematic selection of optimal mobile cranes.

## Literature review

Studies related to crane selection and stability review have been conducted using a wide range of methods. Reddy and Koshy developed a lifting route plan program considering the working radius and lifting capacity of mobile cranes (Reddy and Koshy 2002). Al-Hussein et al. implemented an optimal crane selection algorithm using Visual Basic in consideration of the lifting capacity of mobile cranes (Al-Hussein et al. 2001). However, the studies mentioned above did not consider ground conditions, including the soil bearing force. Tantisevi and Burcu (2007) analyzed and controlled the work space and visual/spatial movement of mobile cranes to minimize friction with other works and delays (Tantisevi and Burcu 2007). This is useful in an effective arrangement and operation of mobile cranes, but it is far from a detailed stability review. Tamate et al. analyzed outrigger loads that cause overturn of mobile cranes. They also conducted an experiment on overturn of mobile cranes as the load is delivered to the outrigger and analyzed the result; however, they did not propose the selection of stability-secured mobile cranes



and plate design algorithms like this study (Tamate et al. 2005). Shapira et al. considered the characteristics of building projects and conducted a study in selecting whether a mobile crane or a tower crane is most suitable. Also, the items to consider in choosing the detailed model (building, site, safety, air, weather, etc.) were analyzed to identify the importance of each item (Shapira and Schexnayder 1999). However, there was no stability review or selection procedure in relation to the items considered. Alkass and Osama developed a simulation program to select cranes by using tools like database management, spreadsheet application programs, graphics, and simulation (Al-Hussein et al. 1997). Similarly, Struková and Ištvaník developed a program to select the optimal location of mobile cranes considering the lifting location, weight and building shape (Struková and Ištvaník 2011). However, there was not enough detailed review on stability of the soil bearing force and the program was aimed at selecting cranes in consideration of lifting conditions such as the weight, height, and building shape.

Furusaka and Gray used the objective function that minimizes rental, installation, and disconnection costs to select an optimal crane, proposing a model that combines various tower cranes (Furusaka and Gray 1984). However, their proposal was not a stability review of mobile cranes. Gray and Little suggested a process of selecting mobile cranes and tower cranes that suit designs at the initial design phase (Gray and Little 1985). However, there was no method of reviewing the stability of the selected cranes or of using the available crane information in the market. Ali et al. studied collision avoidance upon the double lifting of a mobile crane, and Perez et al. developed an algorithm for planning collision-free paths among polyhedral obstacles (Lozano-Pérez and Wesley 1979). Other studies include those conducted by Maczynski and Wojciech, who developed a 3D optimization algorithm of a rotating part to secure rigidity of mobile cranes (Maczynski and Wojciech 2003), and Lin and Haas (1996), who developed a double lifting simulation program (Lin and Haas 1996). These studies did not consider the ground contact stability of mobile cranes. Lastly, Ho et al. studied a method of reviewing the ground contact stability of mobile cranes, but only main items were explained and a formula was proposed (lacking detailed review items and procedure), and no automatic model was proposed (Ho, Seo and Kim 2007). Thus, this study proposes detailed review items and procedure regarding ground contact stability to secure the stability of mobile cranes, and develops an automatic model.

#### **Review process of ground contact stability**

Table 1 shows review items of automatic design algorithms for securing the ground stability of mobile cranes. The review items are divided into review of objects to be lifted,

equipment information, review of ground contact pressure and reinforcement on soil bearing force of flat and sloping site. When examining the ground contact pressure, the maximum reaction of the outrigger is calculated to check stability and the available mobile cranes are identified. When the mobile cranes are selected, the reinforcement of soil bearing force is reviewed based on the ground shape. At the reinforcement planning of soil bearing force of flat site as illustrated in Plate type (steel, timber), rigidity of plate, soil bearing force, and bending moment and shearing force acting on plate should be reviewed. At the reinforcement planning of soil bearing force of sloping site, slope data such as slopping angle, slopping length, slopping height, and distributed load on soil should be examined additionally to design a plate. Here the most optimal plate is designed depending on the crane type and the ground state.

Figure 2 shows the ground contact stability review process. The crane operation plan is classified into reviewing lifting conditions, mobile crane selection, and reviewing ground contact stability. When reviewing lifting conditions, the shape, section, and weight of lifting objects should be checked.

#### **Automatic review and design algorithms**

##### ***Review of basic information in selecting cranes***

The lifting plans and crane selection have complex, dynamic correlations, so the influencing factors include not only the duration and cost in terms of construction management, but also the working radius, work efficiency, interference with nearby buildings and other works, quantity, location selection, site installation, and disconnection, all of which should be taken into consideration (Lin and Haas 1996). The optimal mobile crane is selected considering these factors, and a respective plan should be set by step in order.

For the stability review of mobile cranes, the characteristics, and heights of lifting objects and the distance from a crane should be reviewed as shown in Figure 3. The characteristics of objects to be lifted refer to the shape, weight, and materials, and the crane characteristics indicate the lifting capacity, available lifting height, and turning radius of the boom. These basic factors should be considered when selecting a crane or cranes, and cranes that do not satisfy the given factors are excluded from analyses. In addition, the ground contact stability should be examined based on these factors to prevent overturn of mobile cranes.

##### ***Review of ground contact pressure***

As shown in Figure 4, the ground contact model of this study calculates the maximum ground contact load according to the boom location (A, B, C). The maximum reaction is at the outrigger when the boom is at point B. However, this cannot be seen as the point where the maximum reaction is realized, because B is not the main

Table 1 Review items for ground contact stability

Step	Items reviewed	
Basic Items	Review of the objects to be lifted	Type, material and weight
	Equipment Information	Working radius, the maximum height of objects, crane weight and outrigger radius
Ground contact stability	Review of ground contact pressure	Work direction, ratio of impact load and the maximum reaction of outrigger
	Reinforcement of soil bearing force (flat site)	Plate type (steel, timber), rigidity of plate, soil bearing force, bending moment, and shearing force acting on plate
	Reinforcement of soil bearing force (slopping site)	Additional data including slope data such as slopping angle, slopping length, slopping height, and distributed load on soil

location of the work, and instead is where temporary rotation and passing are demonstrated. Thus, when the boom is located at A (the main location of work), it is regarded as the maximum reaction. Also, considering that the boom rotates at B, 50% of the maximum reaction force should be added for safe design (Ho, Seo and Kim 2007). The formula is as shown in Equations 1 and 2.

When the impact load is not considered:

$$P_{max} = 0.85 \times (W + W_1) \times 0.5 \times 1.5 \tag{1}$$

where  $P_{max}$  is the maximum reaction,  $w$  is the crane weight, and  $W_1$  is the lift weight.

When the impact load is considered:

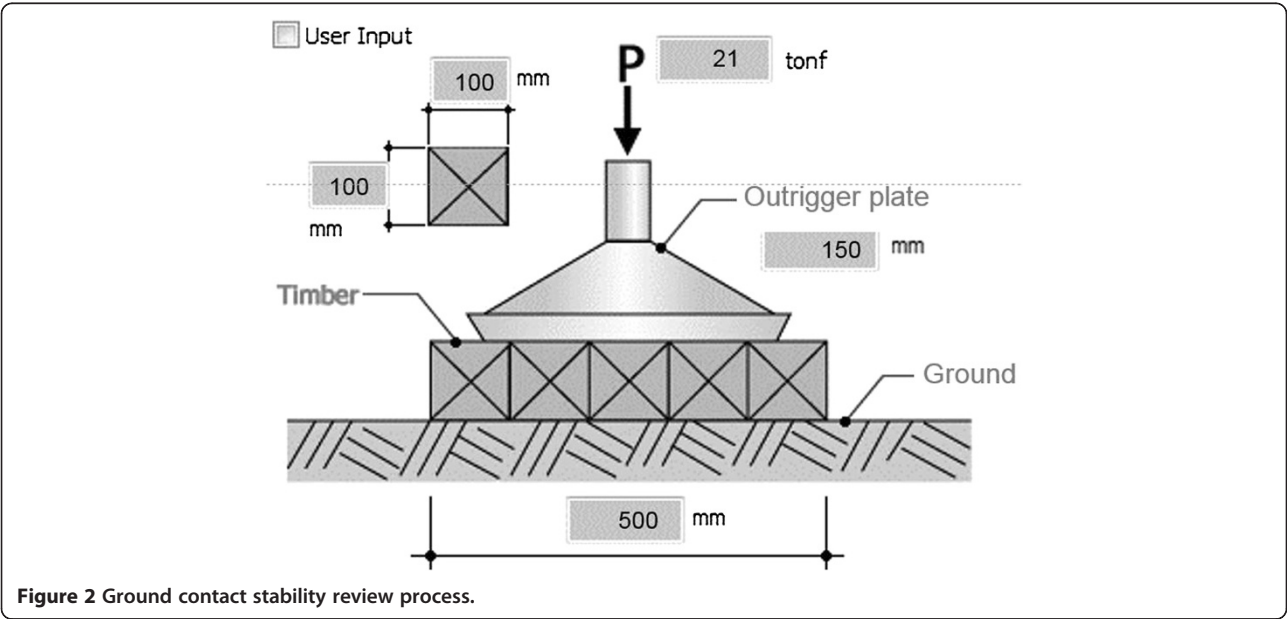
$$P_{max} = 0.85 \times \{(W + W_1) \times 1.3\} \times 0.5 \times 1.5 \tag{2}$$

Figure 5 shows the ground contact stability review process. The crane operation plan is classified into reviewing lifting conditions, mobile crane selection, and reviewing ground contact stability. When reviewing lifting conditions, the shape, section, and weight of lifting objects should be checked. The ground contact pressure

of the outrigger is then reviewed along with the lifting conditions when selecting mobile cranes. This is Simulation 1 proposed in the study. When reviewing ground contact stability, soil bearing force is reviewed based on the results of Simulation 1. Soil bearing force is reviewed separately by flat and slopping site, and each process is developed as in Simulations 2 and 3, respectively.

The generation model for stability review of ground contact stability uses the specifications provided by the crane manufacturer and the project information. Engineers and technicians should set the project information as shown in Figure 6, and the crane information is automatically imported from data that has already been implemented. The ground contact pressure can be examined based on the outrigger span, the turning radius of boom, the body weight, and the lift weight.

The simulation model for automatic stability review of ground contact stability is designed to review all MCs. As illustrated in Figure 7, the simulation model sets the installation location for all MCs and examines the ground contact pressure automatically by the simulation algorithms illustrated in Figure 7.



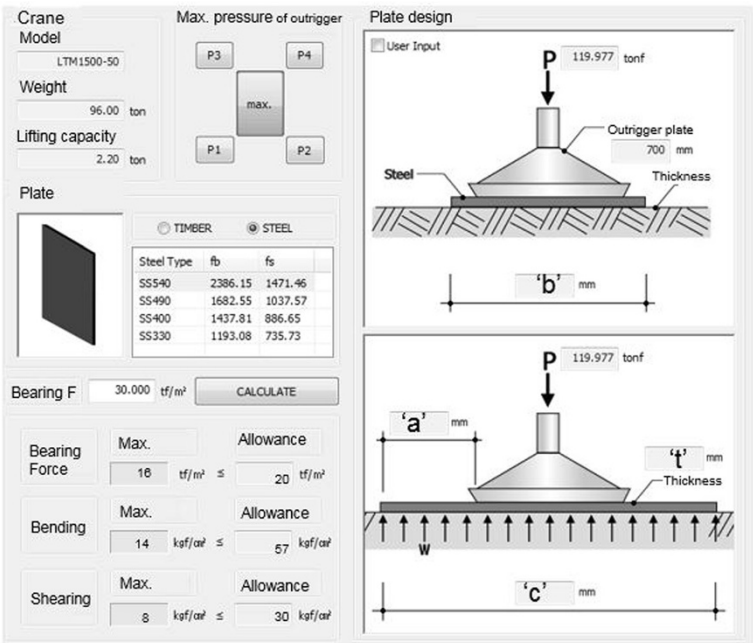


Figure 3 The working radius and height of a mobile crane.

The ground contact pressure is reviewed in the order of the maximum reaction of the outrigger, the working direction and height, and the impact load. The impact load value that is reviewed shows stability through a comparison with the ground conditions. Cranes that are regarded as stable are classified and saved automatically as the candidate

cranes. When all cranes have been reviewed, the simulation examining the ground contact pressure ends.

Reinforcement of Soil Bearing Force (flat site)

After the review of ground contract pressure, the stability of soil bearing force reinforcement should be reviewed to

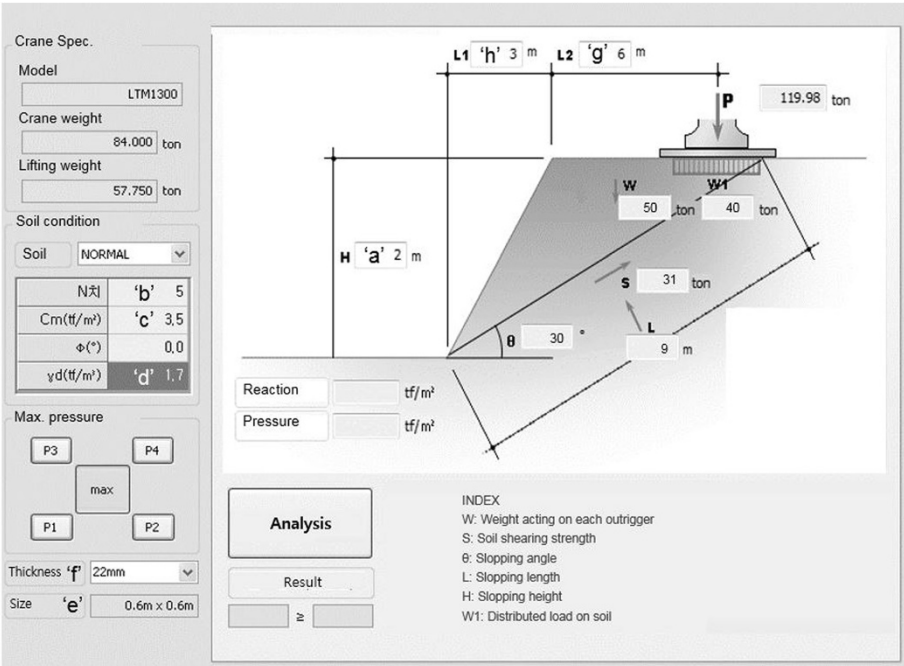
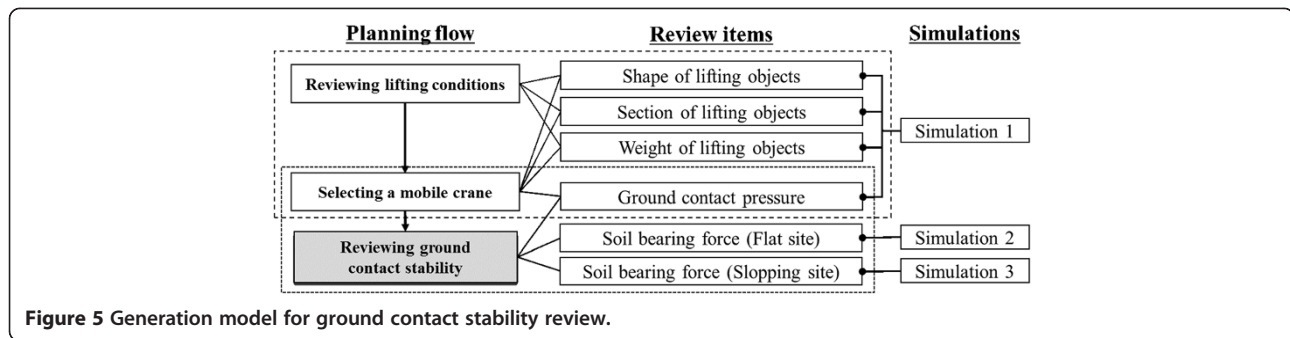


Figure 4 Identification of maximum reaction of a hydraulic crane.





prevent overturn. The reinforcement of soil bearing force is reviewed under 2 different ground conditions: a flat and a slopping site. For the flat site, the plate material, thickness, and area should be reviewed manually by the user as shown in Figure 8 or automatically by the simulation algorithm as shown in Figure 9. Since the plate transfers the ground contact load of the outrigger to the ground, it should be designed after checking the adhesive power and the rigidity of the plate. The plate is usually made of timber and steel, and data including bending and shearing according to the thickness and area should be gathered to be automatically applied to the simulation.

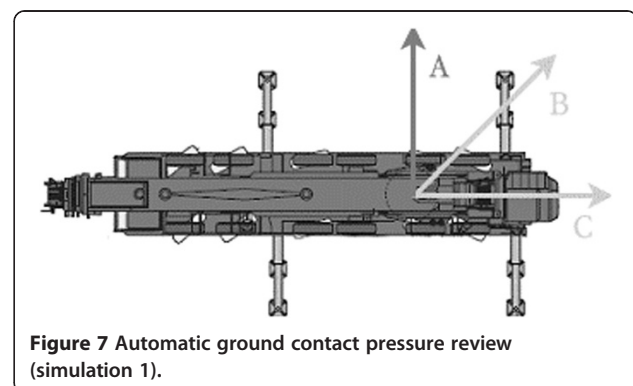
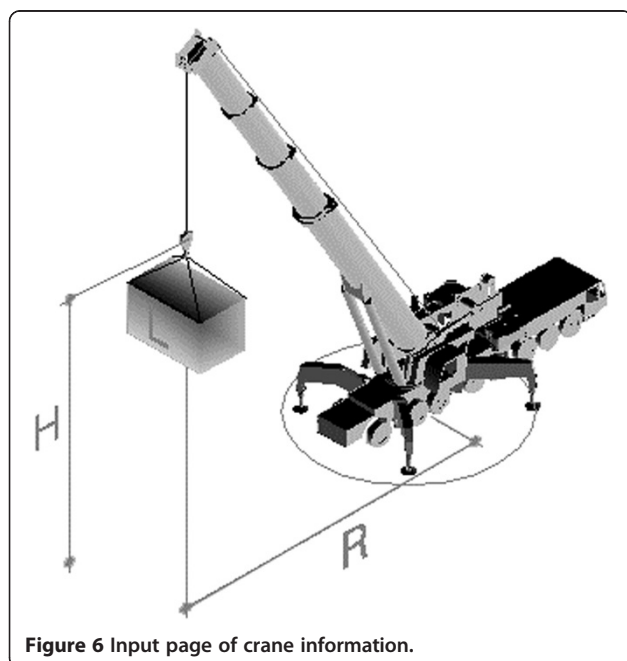
As shown in Figure 10 the generation model of soil bearing force reinforcement as plate reinforcement imports the additional data on ground contact pressure of the outrigger stored in the system implemented by the proposed algorithms besides the basic information specified in Table 1. Based on such data, the plate type, rigidity, bearing soil force, and bending and shearing factors are automatically reviewed for reinforcement of soil bearing

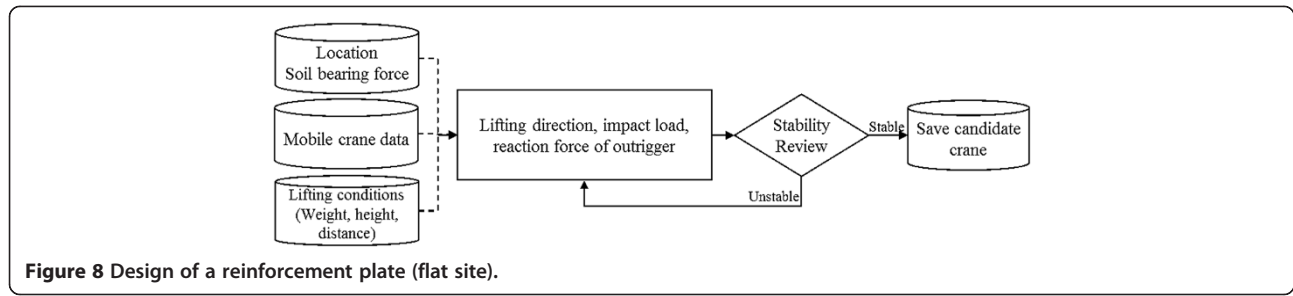
force. When the plate fails to transfer the ground contact load to the ground, the crane is likely to overturn. For a slope, the soil type, soil property value and slope information should also be examined. When stability reviews of all items are completed, the crane and the suitable plate design are saved in pairs.

The automatic plate design for reinforcement of the soil bearing force on a flat site is applied with information like the outrigger of the candidate cranes drawn from simulation 1 as shown in Figure 7 and the body weight. For the plate design in simulation 2, the outrigger of a crane as shown in Figure 9 is selected, and the plate materials and allowable soil bearing force are checked for the design of the materials. The designed plate and the crane are saved in pairs within the scope that stability is secured. Simulation 2 is completed when all the candidate cranes deduced from simulation 1 are reviewed.

As demonstrated in Figure 11, the program automatically reviews the plate design for reinforcement of soil bearing force on a flat site. The rigidity of plates by type and size is imported from the gathered data, and the maximum ground contact load of the outrigger is inserted based on the result of simulation 1. Also, the crane weight and lifting capacity imported from the crane data are inserted. The values are saved after the soil bearing force and the plate's bending and shearing are reviewed.

The plate for reinforcement of soil bearing force on a flat site is divided into timber and steel for the design depending on the material used, and the soil bearing force,





bending, and shearing should be automatically reviewed by the equations (3) to (7). Steel plate review items can be described as follows (Shapiro et al. 2000). Figure 11 shows the variables related to plate design (a, b, c, and t), which should meet the three requirements regarding soil bearing force, bending, and shearing in the automatic design algorithm.

#### Soil bearing force review

$$q = \frac{P}{bc} \leq qa \text{-----O.K} \quad (3)$$

P: Maximum Reaction,  
qa: Allowable Soil Bearing Force

#### Bending review

$$M = \frac{qba^2}{2}$$

$$f1 = \frac{3qa1^2}{t^2} \leq fb \text{-----O.K} \quad (4)$$

$$f2 = \frac{3qa2^2}{t^2} \leq fb \text{-----O.K} \quad (5)$$

M: bending Moment,  
f1: Transversal Bending Stress,  
f2: Longitudinal Bending Stress,  
fb: Allowable Bending Stress,  
a1: Transversal Direction a,  
a2: Longitudinal Direction a,  
t: Thickness of member

#### Shearing review

$$v1 = \frac{1.5qa1}{t} \leq fs \text{-----O.K} \quad (6)$$

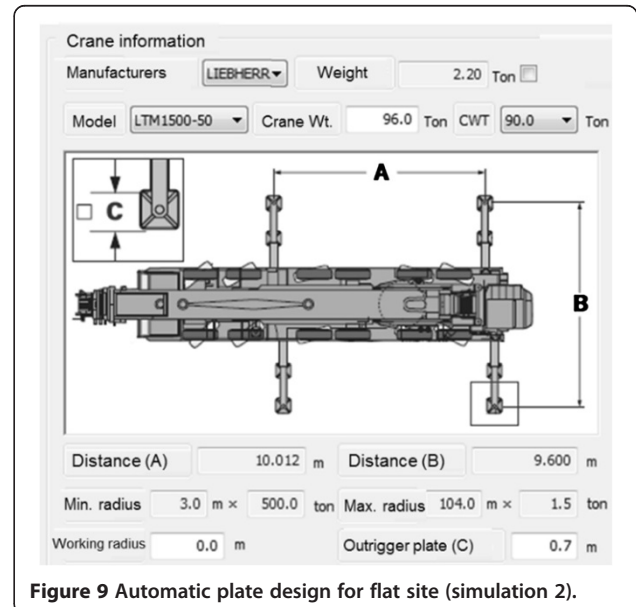
$$v2 = \frac{1.5qa2}{t} \leq fs \text{-----O.K} \quad (7)$$

v1: Transversal, horizontal shear stress  
v2: Longitudinal, horizontal shear stress,  
fs: Allowable shear stress of member

#### Reinforcement of Soil Bearing Force (sloping site)

For the reinforcement of the soil bearing force of a slope, an additional review of the slope shape and the soil property value is required. As shown in Figure 12, the reinforcement plate is designed after reviewing the vertical weight, shearing strength, sliding angle, slope length, and height. The reinforcement plate installed on a slope should consider not only the transfer of load, but also the landslide at the slope.

The plate for reinforcement of the soil bearing force on a slope requires reviews of soil bearing force, bending, and shearing. Steel plate review items are described as follows (Shapiro et al. 2000). Figure 11 shows the variables related



to plate design and slope shape (a, b, c, d, e, f, g, h, and t), and the variables related to plate design (e, f) should meet three requirements regarding soil bearing force, bending, and shearing in the automatic design algorithm.

#### Subgrade reaction (q)

$$q = P_{max} \times n \quad (\text{t/m}^2) \quad (8)$$

#### Reaction area (A)

$$A = \frac{P}{q} \quad (\text{m}^2) \quad (9)$$

Therefore, the longitudinal reaction force  $L3$  is assumed to have a square distribution.

$$L3 = \sqrt{A} \quad (\text{m})$$

$$L2 = g + L3/2 \quad (\text{m}) \quad (10)$$

$$Wa = 1/2 \times d \times a \times L2 \quad (11)$$

$$W = Wa + (q \times L3) \quad (\text{t}) \quad (12)$$

#### Shearing strength S

$$L = \sqrt{(a^2 + (h + L2)^2)} \quad (13)$$

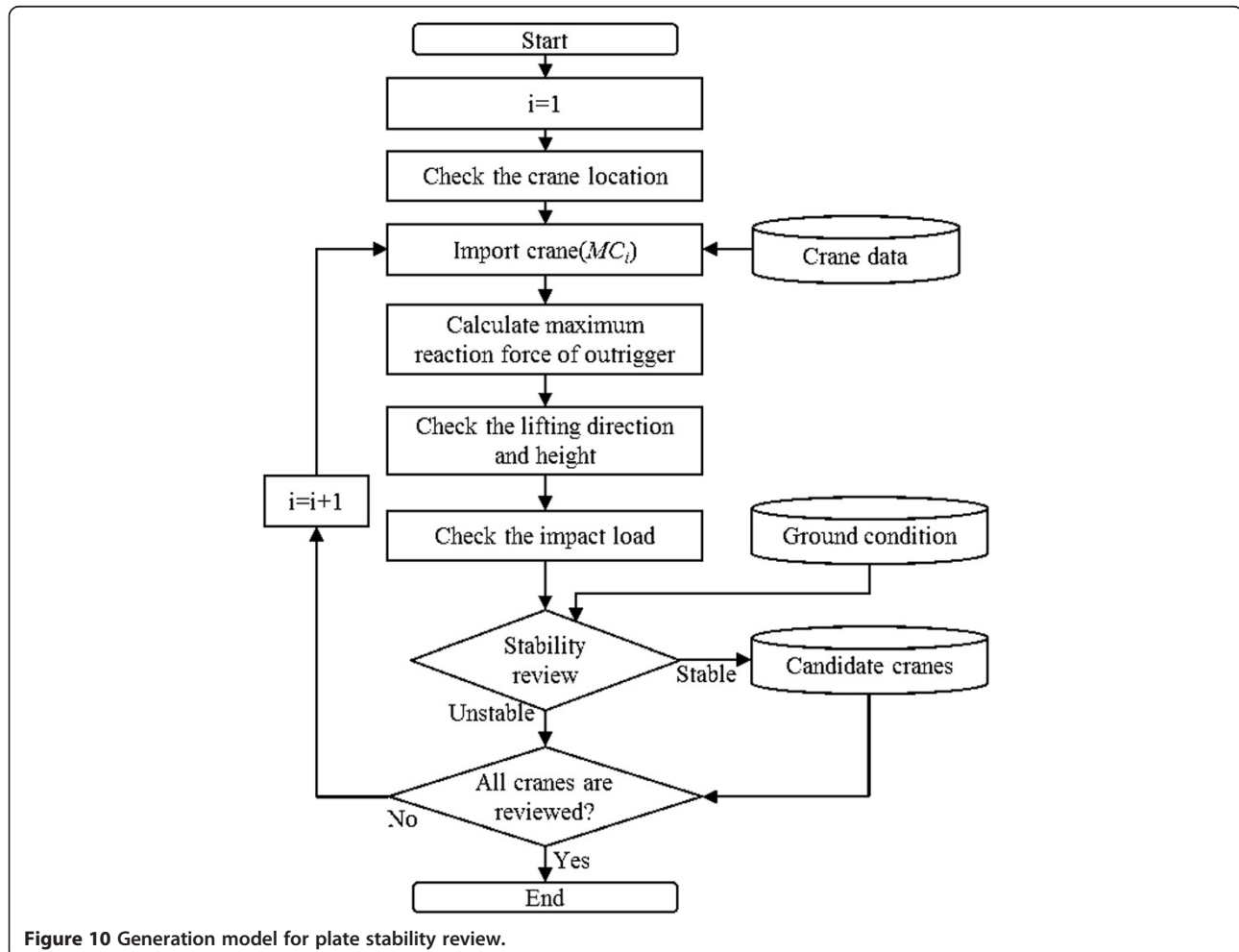
$$\theta = \tan^{-1} \left[ \frac{a}{h + L2} \right] \quad (14)$$

$$S = c \times L + W \cos \theta \times \tan \Phi_m \quad (15)$$

$\Phi_m$ : Friction angle

#### Vertical sliding force

#### Safety angle





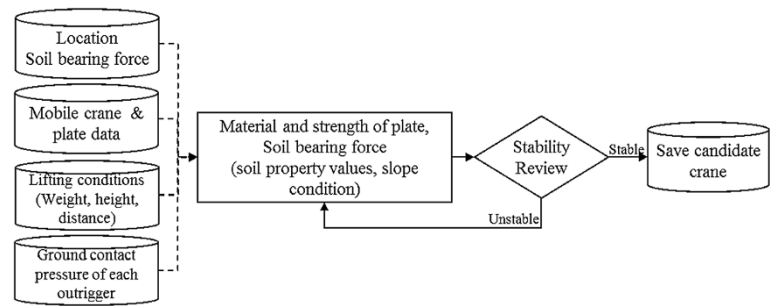


Figure 11 Plate design information (flat site).

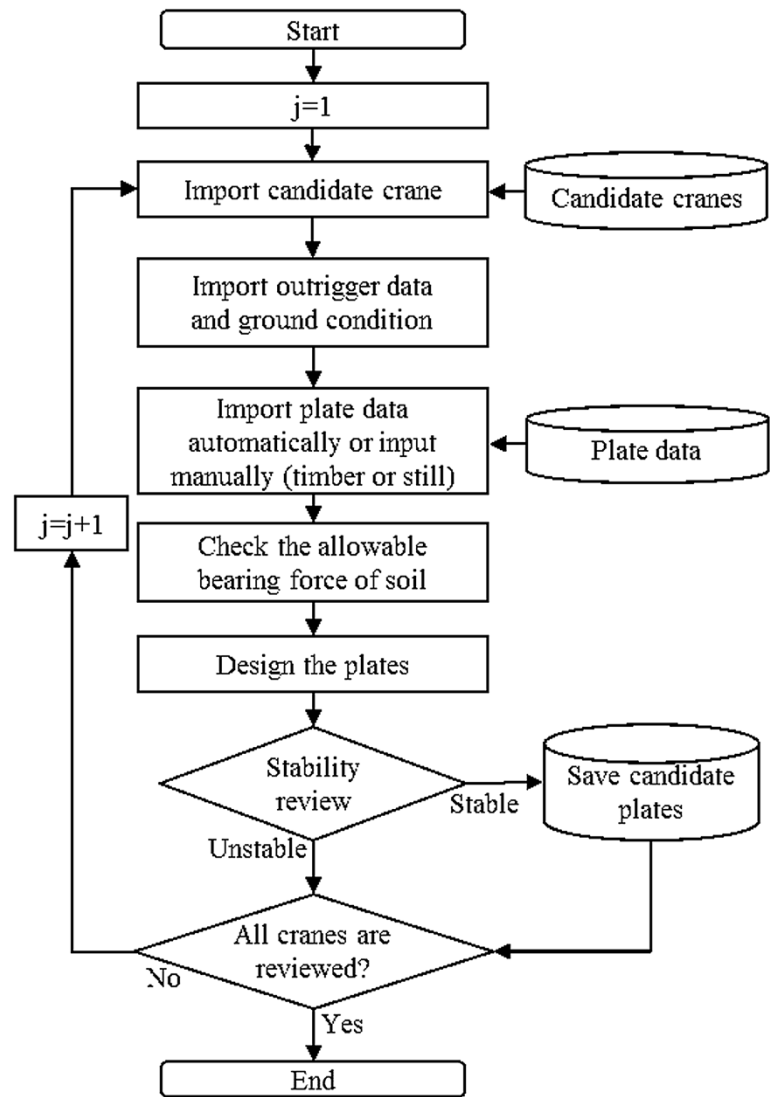
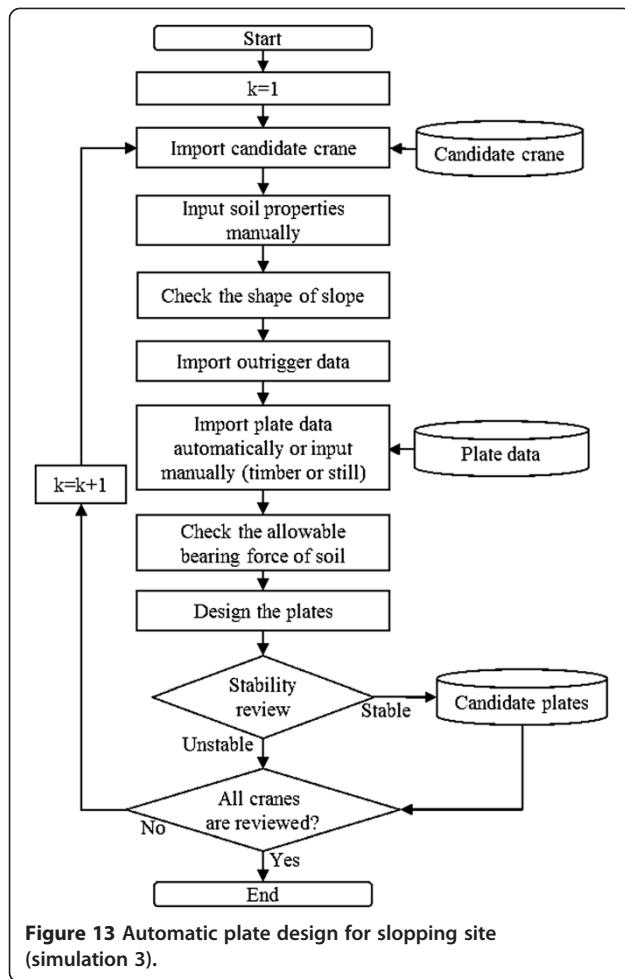


Figure 12 Plate design information (sloping site).



$$Fa = \frac{S}{W \times \sin\theta} > 1.2 \text{-----O.K} \quad (16)$$

As illustrated in Figure 13, the plate design of a slope analyzes the candidate cranes deduced from simulation 1 as illustrated in Figure 7. In simulation 3, the plate is designed by checking the soil properties such as the N value, adhesive power, friction angle, and weight of unit volume that are input manually by the user as shown in Figure 12. Also, the slope shape is automatically analyzed by the equations (8) to (16) to review both the soil bearing force of the soil/ground and the landslide. For the plate design in simulation 3, the outrigger of a crane as shown in Figure 13 is selected, and the plate materials and the allowable soil bearing force are checked for the design of the materials. The designed plate and the crane are saved in pairs within the scope that stability is secured. Simulation 3 is automatically completed when all the candidate cranes deduced from simulation 1 are reviewed.

The top level process for mobile crane plans is comprised of 3 simulations, as illustrated in Figure 14. When

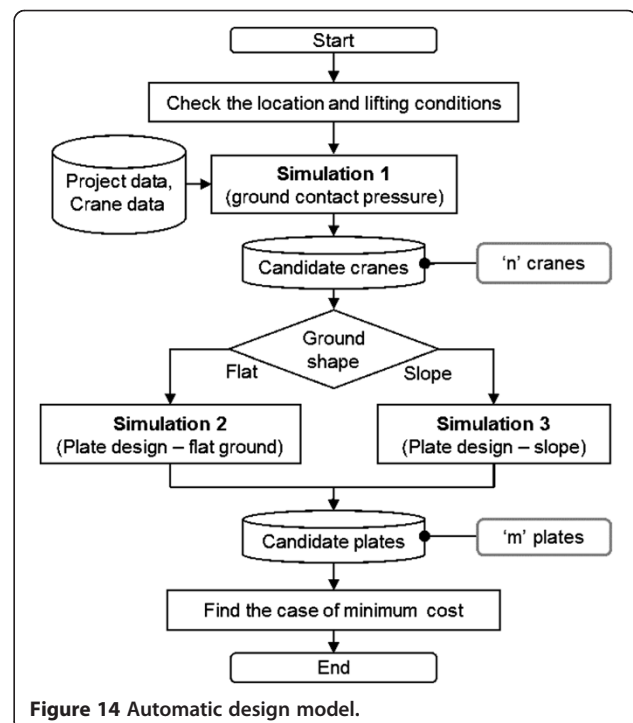
selecting mobile cranes (Figure 7), the project data and crane data are used to deduce the candidate cranes within the required ground contact pressure. It should be checked whether the mobile crane is available in the market, and the selected cranes become the basis for the plate design in simulation 2 or 3.

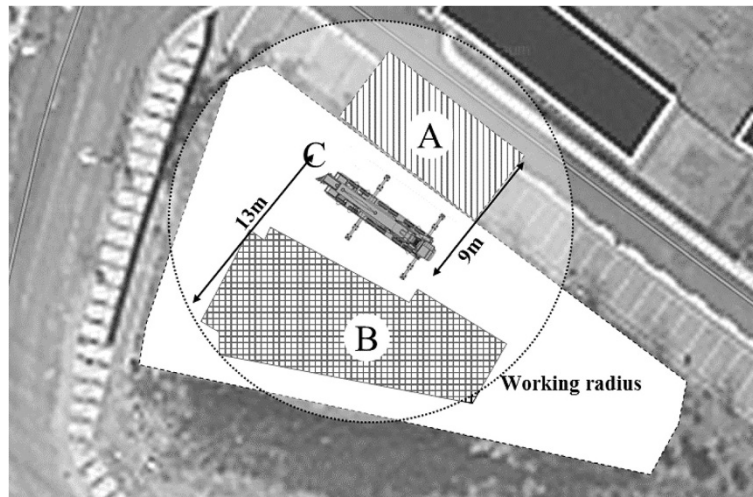
As previously described, only 1 type is simulated according to the ground shape for both simulations (2 & 3), and the plate suitable for the candidate crane is designed. The plate design is paired with the candidate crane for a review of economic feasibility, and is then finally selected.

This study proposes a model for selecting mobile cranes with the lowest cost possible, and designing plates by identifying multiple cases and calculating cost based on securing stability, which is the prerequisite. The objective variable of mobile crane and plate design is cost ( $C_{mc}$ ). The objective function of this model is to minimize the sum of mobile crane rental cost ( $C_{rental}$ ) and plate cost ( $C_{plate}$ ) as shown in Formula 17. The cost calculation of the model shown in Figure 14 is automatically carried out in 2 steps. First, a rental cost is calculated from the data of n candidate cranes. Second, respective cost is calculated for 'm' plates designed in simulations 2 and 3. The model aims to estimate the minimum cost, and the objective and constraint functions are as shown below.

$$\text{Minimize} \{ C_{mc} \} \quad (17)$$

$$C_{mc} = C_{rental} + C_{plate}$$





**Figure 15** Site of case study project.

Subject to:  $WR_{mc} \geq$  required working radius

$LC_{mc} \geq$  required lifting load

$MI_{outrigger} \leq$  allowable bearing force of soil

$SH_{plate} \geq$  shear force of plate

$BE_{plate} \geq$  bending force of plate

Where  $C_{mc}$ : cost of mobile crane work

$C_{rental}$ : rental cost of mobile crane

$C_{plate}$ : cost of designed plate

$WR_{mc}$ : working radius of selected mobile crane

$LC_{mc}$ : lifting capacity of selected mobile crane

$MI_{outrigger}$ : maximum impact load of outrigger

$SH_{plate}$ : allowable shear stress of designed plate

$BE_{plate}$ : allowable bending stress of designed plate

## Result and discussion

To verify the effectiveness of the automatic design model, a case project is selected and the algorithm is applied assuming several conditions. Above all, the case project is a site where buildings are not completed, and it is assumed that PC members are to be installed on the first floor. C in Figure 15 is the location of a mobile crane, and A shows a material storage yard. B is the building to be constructed, and the distance between a crane and a building is around 13 m. The heaviest lifting object is the PC beam that is 8 m long, which weighs 4.6 tons. The total lifting weight considering sling and lug is 5.06 tons.

In consideration of lifting conditions such as the working radius and weight of lifting objects, 18 candidate cranes are selected in total. Ground contact pressure upon operation of each candidate crane is calculated, and allowable soil bearing force is set as 20 tf/m<sup>2</sup> to design plates for reinforcement of soil bearing force.

As a result no information regarding self-weight, so they are not automatically designed. a, b, c, and t in Table 2 refer to the width, breadth and thickness of plates shown

in Figure 3. Ground contact pressure increases in the case of large cranes due to their self-weight, and they are designed with width and breadth of 2500 mm. This restricts the use of cranes. The smallest plate is designed with width of 1000 mm and thickness of 24 mm.

When the allowable soil bearing force is set as 30 tf/m<sup>2</sup> under the same lifting conditions, plate design is as described in Table 3. Applicable crane types are the same, yet plate design has changed. Due to the difference in allowable soil bearing force, the plate for reinforcement of soil bearing force is designed with width and breadth of 800 mm and thickness of 15 mm. Thus, the specifications in Table 3 should be applied for reinforcement plates when using cranes to limit crane overturn risks.

## Conclusion

This study develops automatic design algorithms for securing the ground contact stability of mobile cranes. In addition, the algorithms proposed in the study focus on the ground stability review process of mobile cranes. The study subjects are hydraulic cranes (or tire cranes), and single lifting is assumed for the study. Ground contact stability is reviewed based on the installation of cranes on soil or ground.

The study results are as follows.

Firstly, we found that the database built using the available tower cranes in the market for automatic design of mobile cranes can easily and quickly select candidate cranes according to lifting conditions and design plates through simulations.

Secondly, design components required for ground contact plate design are collected to build the database, which allows easier and quicker stability review. Moreover, automatic design algorithms are capable of obtaining optical

**Table 2 Result of automatic design model (1)**

Mobile crane	Capacity (ton)	Ground contact pressure (ton)	Steel plate			
			a (mm)	b (mm)	c (mm)	t (mm)
TM1500	80	58.786	570	1750	1750	34
TG1500E	150	-	-	-	-	-
TG1000E	100	-	-	-	-	-
TG800E	80	33.316	420	1300	1300	26
TG8500EX	50	27.451	400	1200	1200	24
TG300E	30	-	-	-	-	-
SC50H	50.5	33.316	400	1200	1200	24
SC25H	25	27.451	300	1000	1000	18
LTM1500-84	500	121.801	900	2500	2500	54
LTM1500-50	500	121.801	900	2500	2500	54
LTM1400	400	124.988	900	2500	2500	54
LTM1300	300	114.151	900	2400	2400	54
LTM1200	200	87.376	750	2100	2100	45
LTM1160	160	73.351	670	1950	1950	40
LTM1120	120	43.516	450	1500	1500	27
LTM1090	100	46.576	520	1550	1550	31
LTM1070	70	40.647	470	1450	1450	28
LTM1060	70	39.245	470	1450	1450	28

**Table 3 Result of automatic design model (2)**

Mobile crane	Capacity (ton)	Ground contact pressure (ton)	Steel plate			
			a (mm)	b (mm)	c (mm)	t (mm)
TM1500	80	58.786	390	1400	1400	29
TG1500E	150	-	-	-	-	-
TG1000E	100	-	-	-	-	-
TG800E	80	33.316	320	1100	1100	23
TG8500EX	50	27.451	300	1000	1000	21
TG300E	30	-	-	-	-	-
SC50H	50.5	33.316	300	1000	1000	22
SC25H	25	27.451	200	800	800	15
LTM1500-84	500	121.801	670	2050	2050	49
LTM1500-50	500	121.801	670	2050	2050	49
LTM1400	400	124.988	720	2050	2050	53
LTM1300	300	114.151	700	2000	2000	50
LTM1200	200	87.376	570	1750	1750	42
LTM1160	160	73.351	500	1600	1600	36
LTM1120	120	43.516	320	1250	1250	23
LTM1090	100	46.576	370	1250	1250	28
LTM1070	70	40.647	350	1200	1200	25
LTM1060	70	39.245	320	1150	1150	24

design plans from among those that satisfy stability review requirements after relevant costs are calculated.

Lastly, a plate design model connected to the selected mobile crane should first review ground contact pressure. It was found that system runtime is shortened when ground contact pressure to prevent overturn is reviewed before design.

The algorithms proposed in this study conduct simulations for all possible candidate cases, save the results in a database, review practical alternatives, and select the solution that minimizes cost. This is because stability is more important than economic feasibility when operating mobile cranes. Developed processes are useful for analyzing correlations of mobile crane performance, ground contact and soil bearing force reinforcement designs and so forth, and for systematically selecting optimal mobile cranes. Other studies should be conducted on stability review models of double lifting (where 2 mobile cranes are used). Furthermore, stability review models of components such as the sling and lug required for lifting must be developed to prevent the fall of lifting objects.

#### Competing interests

The algorithms proposed in this paper demonstrate the review for securing the ground contact stability and the design of reinforcement plates automatically after a mobile crane selection. The case study was carried out to verify the effectiveness of the proposed algorithms.

Many researchers have conducted a wide range of studies about mobile cranes such as the implementation of a lifting route plan program (Reddy and Koshy 2002; Lozano-Pérez and Wesley 1979) and a crane selection algorithm (Al-Hussein et al. 2001; Shapira and Schexnayder 1999; Al-Hussein et al. 1997; Furusaka and Gray 1984; Gray and Little 1985), the overturn analysis of outriggers (Tamate et al. 2005), the friction with other works (Tantisevi and Burcu 2007) and even the development of a dual lifting simulation program. However, they didn't deal with a series of mobile crane management for securing both stability and economy, but dealt with the partial issue of it, whereas this paper covered the principal issues from selecting a proper crane responding to the lifting conditions to reviewing the stability of cranes automatically, followed by the economic design of reinforcement plates.

The case study of this paper illustrates the automatic reinforcement plate design for two cases of allowable soil bearing force. Site engineers can figure out the rental and plate costs of candidate cranes and, then, select the minimum cost for crane operation. A series of algorithms for mobile crane management was implemented to the software for practical use except the cost minimization algorithm that should be additionally equipped to the software for better use in practice.

#### Authors' contributions

DL and SK together carried out the field study. Subsequently, the gathered data was analyzed. All authors contributed to develop the algorithms. All authors read and approved the final manuscript.

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